# Near flow measure **15 found** the future **is found** lidars:



ZephIR Dual-Mode

5-beam Avent demonstrator

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# Searching for free stream wind speed





- Decorrelation WSpeed / power
- H<sub>hub</sub> speed insufficient?

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- 2.5D not really free wind ...

#### Does this make it any easier?





- In complex terrain:
  - -any "free stream" wind speed idea?
  - -site calibration? Maybe

#### Does this make it any easier?



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- Offshore:
  - -mast expensive
  - -free wind may not be measurable due to wakes

# Power performance verification: nacellemounted lidars, the future?



- Several possibilities for lidar measurements:
- 1) <u>2.5D distance</u> fitting wind speed + direction + shear to lidar-measured LOS velocities



# Power performance verification: nacellemounted lidars, the future?



• Several possibilities for lidar measurements:



#### Case 1: lidar meas. @2.5D



#### **5B-Demo**: use the 5 pts **ZDM**: use 10 pts



#### Case 1: lidar meas. @2.5D Mast comparison



#### **5B-Demo**: use the 5 pts

ZDM: use 10 pts

HWS estimated @hub height



#### Case 1: lidar meas. @2.5D Power curves





#### Case 2: lidar meas. @ multiple distances close to rotor



**5B-Demo** : use the 5 pts @[0.5 0.75 1.0 1.15] D

**ZDM**: use 10 pts @[0.3 1.0 1.25] D



Case 2: lidar meas. @ multi-dist (near flow) Mast comparison

**5B-Demo**: use the 5 pts @[0.5 0.75 1.0 1.15] D

**ZDM**: use 10 pts @[0.3 1.0 1.25] D

HWS estimated @hub height and @2.5D distance



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#### Case 2: lidar meas. @ multi-dist (near flow) Power curves

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## **AEP results**

- IEC -12-1 methodology
- extrapolated AEPs
- 0.5 m/s bin width
- Relative difference in % of cup-based AEP

Lidar measurements	@2.5 D (case 1)			<b>@multiple distances</b> (case 2)		
Rayleigh avg wind speed	6 m/s	8 m/s	10 m/s	6 m/s	8 m/s	10 m/s
Avent 5-Beam demonstrator lidar	Wspeed difference: +1.2%			Wspeed difference: +0.1%		
	-2.0%	-1.6%	-1.2%	-0.4%	-0.1%	+0.0%
Zephir Dual Mode lidar	Wspeed difference: +0.1%			Wspeed difference: -0.7%		
	+0.4%	+0.2%	+0.1%	+2.0%	+1.3%	+0.9%

→AEP estimations as good with the "multi-distances" method as with the 2.5D (<1.5% difference)</p>



#### Take-aways



- $V_{\infty}$  is found! The solution: measurements close to rotor, within the induction zone, at multiple distances, e.g. with nacelle lidars
- Wind Field Reconstruction algo. provide estimates comparable classic mast instrumentation (< 1% difference)
- Power curves in flat terrain verified accurately, reduced scatter (as usual with nacelle lidars)
  - →next generation of IEC61400-12-1 standards? (NWIP)

#### • Further work :

- -Two-dimensional induction? (ongoing)
- Adaptation and testing of method in complex terrain (campaign in Hill of Towie, Zephir DM+4-beam Wind Iris)
- Uncertainty assessment of Wind Field Characteristics: speed, direction, shear, induction factor / Ct, ...

# Thanks for your attention!





More info:

- website <u>www.unitte.dk</u>
- contact <u>borr@dtu.dk</u>







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Doppler wind LiDaRs do not...

...measure wind speed, wind direction, shear, ...

see Hardesty, 1987 (wonderful description of lidar principles)

- They:
  - only measure LOS velocities

–estimate/reconstruct wind field characteristics (WFC)



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#### Modelling the wind field

- choose a wind model that fits the application & site characteristics
- the reconstruction should be performed either in the WIND coordinate systems or in the HUB

#### For power performance: static models

- -i.e. no time dependency
- -use 10-min averages of:
  - LOS velocities
  - inclinometers readings
- use knowledge of the trajectory (opening angles, ranges config) and of lidar position



#### Wind models

Model	U	V	W	comment
Homogeneous 2D	$U_w = cst  \leftrightarrow U_I = U$	$V_w = 0 \iff V_I = V$	$W_w = 0 \iff W_I = 0$	Does not depend on X, Y, Z
Homogeneous 3D	$U_w = cst  \leftrightarrow U_I = U$	$V_w = 0 \iff V_I = V$	$W_w = 0 \iff W_I = W$	Does not depend on X, Y, Z
Inhomogeneous 2D + linear V shear	$U_w = v_0 + \delta_V \cdot (z_W - z_{hub})$ $\leftrightarrow U_I = f(z)$	$V_w = 0 \iff V_I = V$	$W_w = 0 \iff W_I = 0$	Yaw misalignment $\alpha_H = cst$
Inhomogeneous 2D + linear V shear + linear V veer	$U_w = v_0 + \delta_V \cdot (z_W - z_{hub})$ $\leftrightarrow U_I = f(z)$	$V_w = 0 \iff V_I = f(z)$	$W_w = 0 \iff W_I = 0$	Yaw misalignment $\alpha_H = f(z)$
Inhomogeneous 2D + power law shear	$U_w = v_0 (z_w/z_{hub})^{\alpha_{exp}}$ $\leftrightarrow U_I = f(z)$	$V_w = 0 \iff V_I = V$	$W_w = 0  \leftrightarrow W_I \\ = 0$	Yaw misalignment $\alpha_H = cst$



- $\circ$  HWS  $v_0$
- o yaw misalignment  $\alpha_H$  (relative wind dir)
- o shear exponent  $\alpha_{exp}$
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#### Wind models

Model name	U	V	W	comment
Homogeneous 2D	$U_w = cst  \leftrightarrow U_I = U$	$V_w = 0 \iff V_I = V$	$W_w = 0 \iff W_I = 0$	Does not depend on X, Y, Z
Homogeneous 3D	$U_w = cst  \leftrightarrow U_I = U$	$V_w = 0 \iff V_I = V$	$W_w = 0 \iff W_I = W$	Does not depend on X, Y, Z
Inhomogeneous 2D + linear V shear	$U_{w} = v_{0} + \delta_{V} \cdot (z_{W} - z_{hub})$ $\leftrightarrow U_{I} = f(z)$	$V_w = 0 \iff V_I = V$	$W_w = 0 \iff W_I = 0$	Yaw misalignment $\alpha_H = cst$
Inhomogeneous 2D + linear V shear + linear V veer	$U_{w} = v_{0} + \delta_{V} \cdot (z_{W} - z_{hub})$ $\leftrightarrow U_{I} = f(z)$	$V_w = 0 \iff V_I = f(z)$	$W_w = 0 \iff W_I = 0$	Yaw misalignment $\alpha_H = f(z)$
Inhomogeneous 2D + power law shear	$U_w = v_0 (^{z_w} / _{z_{hub}})^{\alpha_{exp}}$ $\leftrightarrow U_I = f(z)$	$V_w = 0 \iff V_I = V$	$W_w = 0 \iff W_I = 0$	Yaw misalignment $\alpha_H = cst$
Inhomogeneous 2D + power law shear + induction model	$U_w = f(x, z)$ $\leftrightarrow U_I = f(x, z)$	$V_w = 0$ $\leftrightarrow V_I = f(x, z)$	$W_w = 0 \iff W_I = 0$	1D Biot- Savard for induction fct

fitted wind characteristics are: free stream HWS  $U_{\infty}$ , yaw misalignment  $\alpha_{H}$ , shear exponent  $\alpha_{exp}$ , induction factor a.

# Power performance verification: "standard" procedure, what's the problem?



- Decorrelation WSpeed / power
- H<sub>hub</sub> speed insufficient?
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- 2.5D not really free wind ...
- Too expensive: e.g. offshore

Power performance verification: "standard" procedure, what's the problem?

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# Nørrekær Enge campaign (NKE), 7 months



- Two nacelle lidars: Avent 5-beam (5B) in blue, ZephIR Dual Mode (ZDM) in red
- IEC compliant mast + SCADA + full loads



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# Power performance verification: nacellemounted lidars, the future?



• Several possibilities for lidar measurements:



# A simple induction model

#### Derived from the Biot-Savart law

- -See The upstream flow of a wind turbine: blockage effect
- -two parameters: induction factor  $a_{,}$  free wind speed  $U_{\infty}$

$$\frac{U}{U_{\infty}} = 1 - a \left( 1 + \frac{\xi}{\sqrt{1 + \xi^2}} \right), \text{ with } \xi = \frac{x_W}{R_{rot}}$$

What does the induction looks like in NKE?



Black: theoretical, a = 0.3Colored lines: different 10min periods

Fitting *a* and  $U_{\infty}$  should be possible